

Headquarters U.S. Air Force

Integrity - Service - Excellence

Thermal Source Reduction Technologies



U.S. AIR FORCE

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Thermal Technologies

- **Steam injection**
- **Resistive heating**
 - **3- or 6-phase heating**
- **Hot air injection**
- **Heat wells/blankets**
- **Radio frequency heating**
- **Hot water flushing**



Recovery Systems

GW

Technology

SVE

Extraction

Steam injection

✓✓

✓

Resistive heating

3- or 6-phase heating ✓✓

Hot air injection

✓✓

Radio frequency heating ✓✓

Hot water flushing

✓✓

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Overriding Equation

IF:

A = (Complex lithology)

B = (Complex soil:water:NAPL:vapor interactions)

C = (Complex resistive heating)

D = (Complex heat dissipation)

E = (Complex condensate deposition)

F = (Complex soil conductivity/permeability changes)

G = (Complex vapor recovery)

H = (Complex aboveground treatment and controls)

THEN: $A \times B \times C \times D \times E \times F \times G \times H = ?$



Resistance Heating

- **Resistance controlled by electrical conductivity, soil moisture**
- **These parameters are likely to change significantly over time and space**
- **Soil moisture supports more efficient resistive heating, but can interfere with effective vapor capture and treatment**



Soil Conductivity

- **Example:**
 - **Lower conductivity clay - 29 Ω**
 - **Higher conductivity clay - 2.5 Ω**
- **For a 20 kW power input (100 A):**
 - **The lower conductivity clay would require a line voltage of 440 V (RMS)**
 - **The higher conductivity clay would require a line voltage of 115 V (RMS)**



Power Delivery

If a sand were to uniformly dry out from $s = 5 \times 10^{-3}$ S/m (18% moisture) to 1×10^{-4} S/m (50x),

Then the resistance would climb by a factor of 51W to 2,600W

For a constant voltage source, the interelectrode current would decrease by the same factor, reducing the power delivered to the soil by a factor of $(51)^2 = 2,600$



Power Dissipation

- **50% of power dissipated within 5 inches of electrodes**
- **8% within carbon particle-filled annulus surrounding each electrode**
- **“Rapid soil drying of the soil would be expected with a corresponding significant increase in R_{total} , and this was observed.” (Dablow et. al. 2000)**



Power/Heat Dissipation

- **Mineral encrustation of irrigated electrodes caused a decrease in electrical power transfer** (Dablow et. al. 2000)

- **Heating vs. vapor capture area**
 - **Practitioners estimate that heating extends to approximately 140% of the electrode array area**



Steam Generation

- **In situ:**
 - **Resistive heating & Hot air injection**
 - **Vadose zone: 40 - 90L H₂O/m³ soil**
 - **Saturated zone: 200 - 400L H₂O/m³ soil**
- **Ex situ:**
 - **Steam injection**
- **Latent heat of vaporization of water [2.45MJ/L]**



Vapor Capture

- **The subsurface is an excellent heat exchanger**
- **Steam condensate will be formed between any steam generation point A and point B where soil temperatures are $< 100^{\circ}\text{C}$**
- **Air permeability is reduced to near zero in areas of high water saturation (e.g. $< 60\%$)**
- **“Flash” volatilization instantaneously creates large increases in volume**



Tracer Recovery Tests

- **Essential to vapor capture efficiency evaluation**
 - **Air Force Plant 4 -**
 - **Helium recovery tests resulted in 3 - 92% He recovery prior to heating**
 - **Two helium injection points within screened interval of SVE wells**
 - **One helium injection point 2- 3 feet below SVE well = lowest recovery**
 - **Problem quantifying He in “hot, humid” stream**
 - **Did not evaluate total recovered**
-



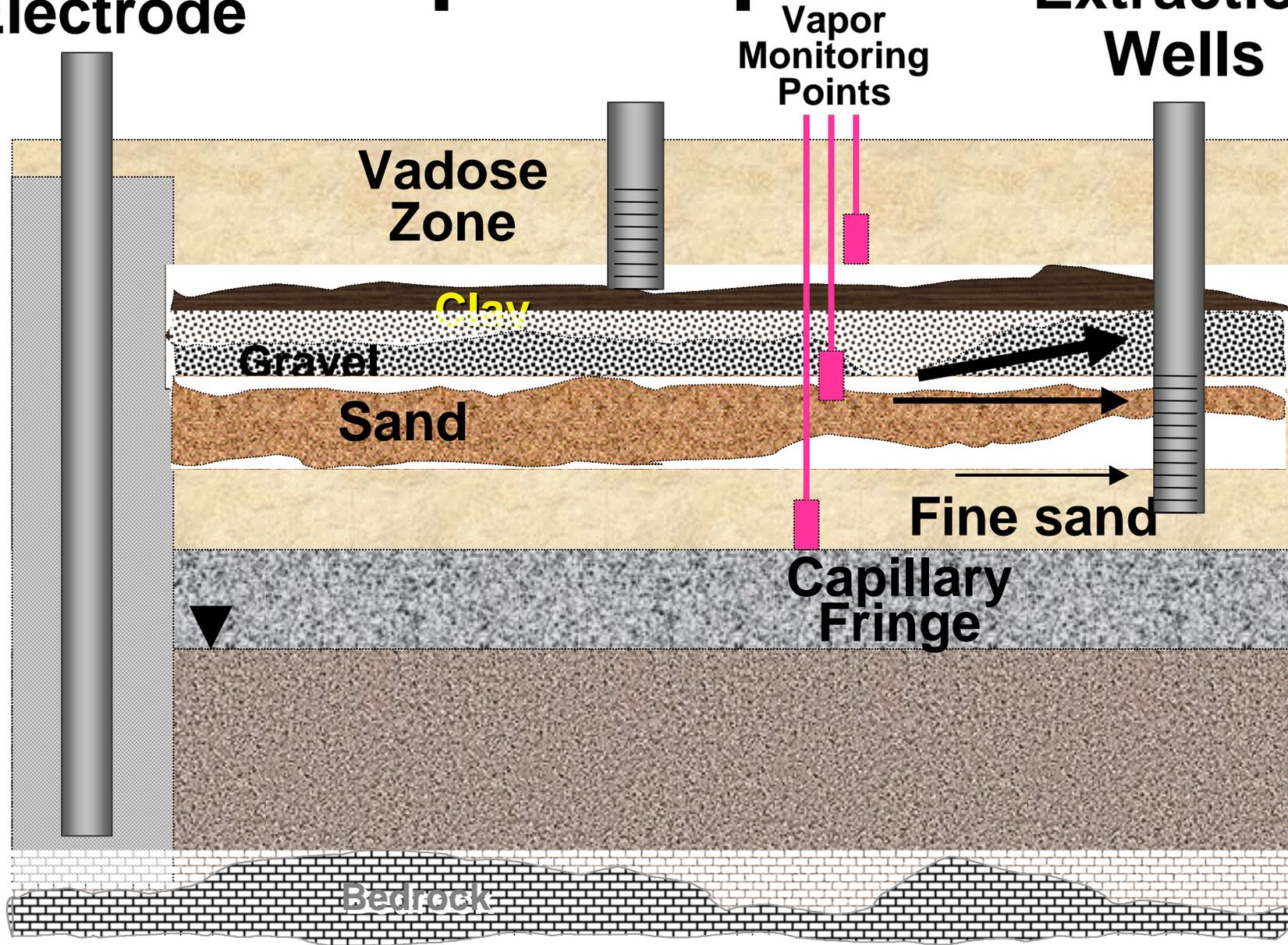
Helium Recovery

Monitoring Point	Extracted Gas Flowrate (SCFM)			Helium Recovery (%)		
	Baseline	Week 4	Week 9	Baseline	Week 4	Week 9
TA-12	13.8			25		
Main Header	111.9			92		
VR-3d	15.3	12.1	13.7	37	55	58
Main Header	111.7	120.1	163.3	45	87	74
TA-13		12.4	16.8		22	80
Main Header		122.1	163.3		88	105
VR-2s	7.0			3		
Main Header	112.1			69		
VR-2d		10.1	10.5		161	259
Main Header		118.4	165.1		120	96

**Heating
Electrode**

Vapor Capture

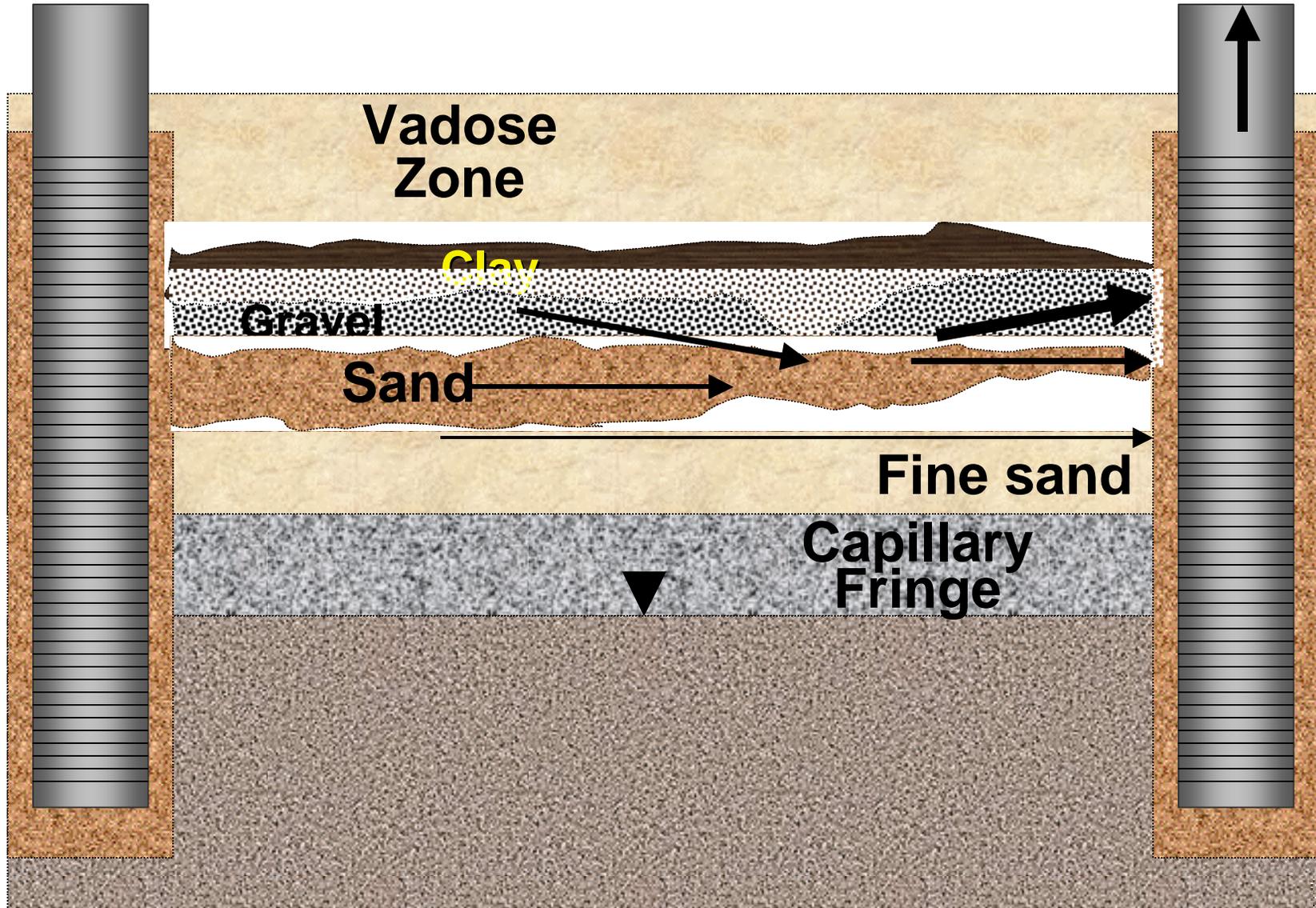
**Vacuum
Extraction
Wells**



**Steam
Injection**

SVE Only

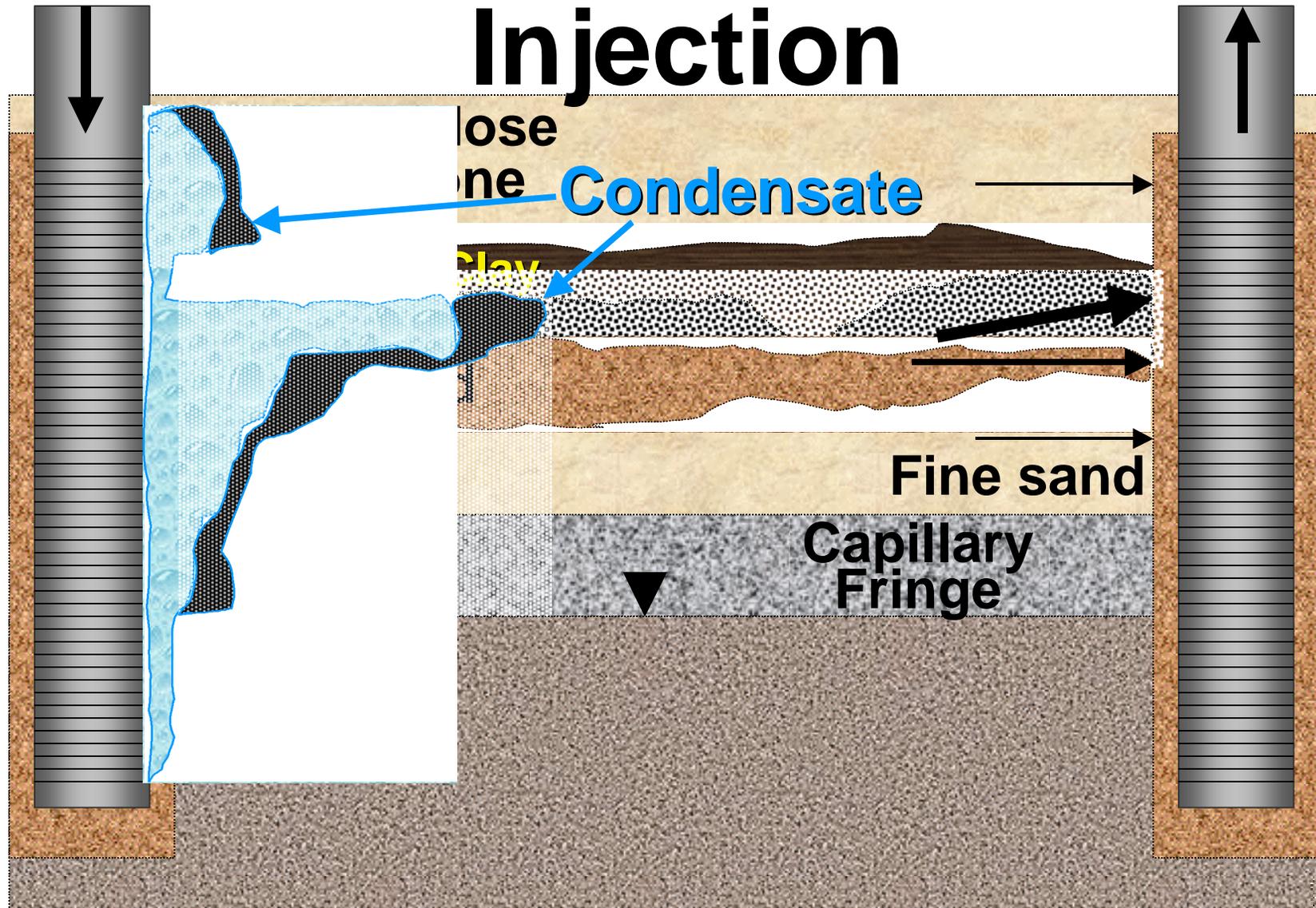
**Vacuum
Extraction**



Steam Injection

Early Steam Injection

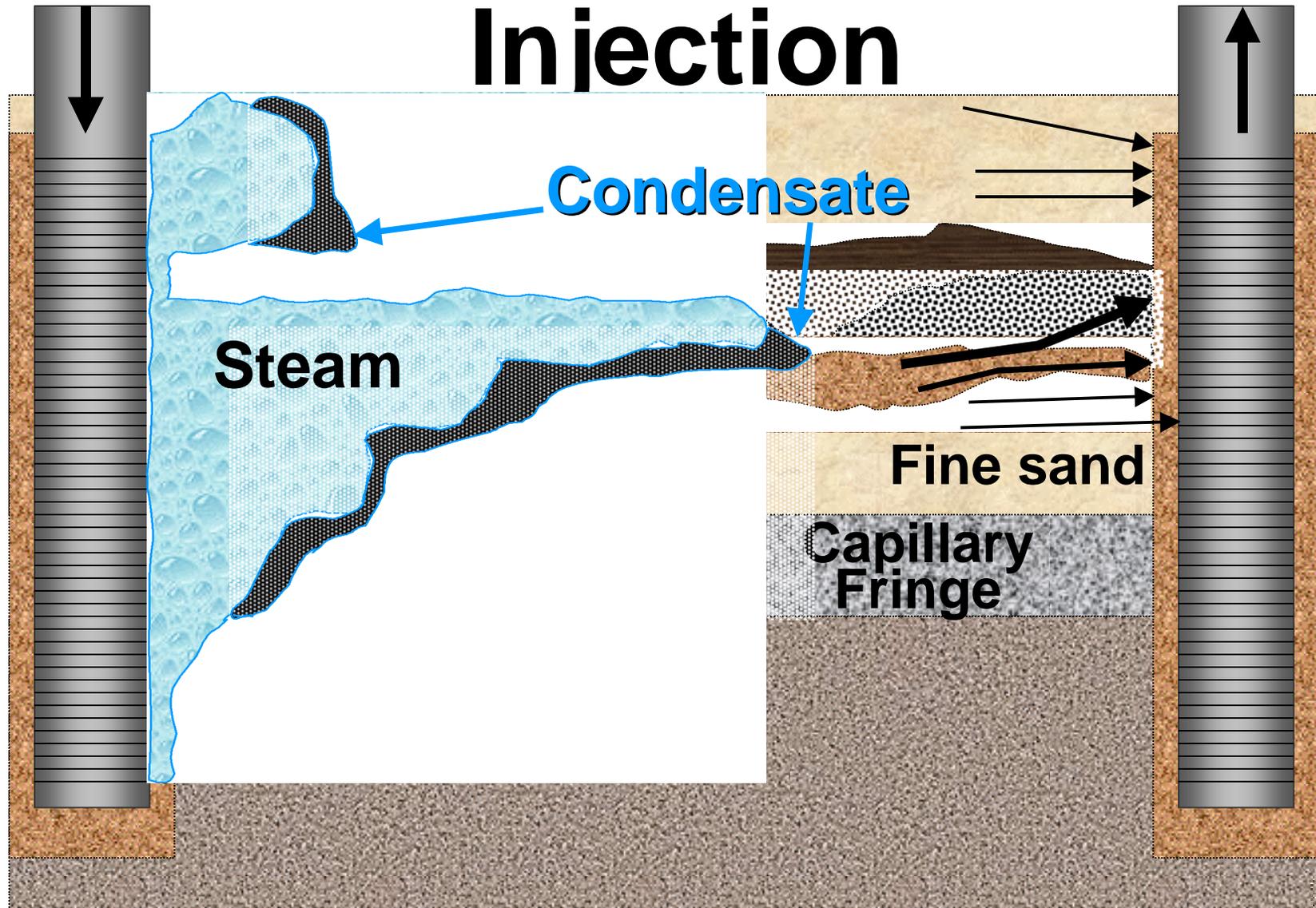
Vacuum Extraction



**Steam
Injection**

Mid-Steam Injection

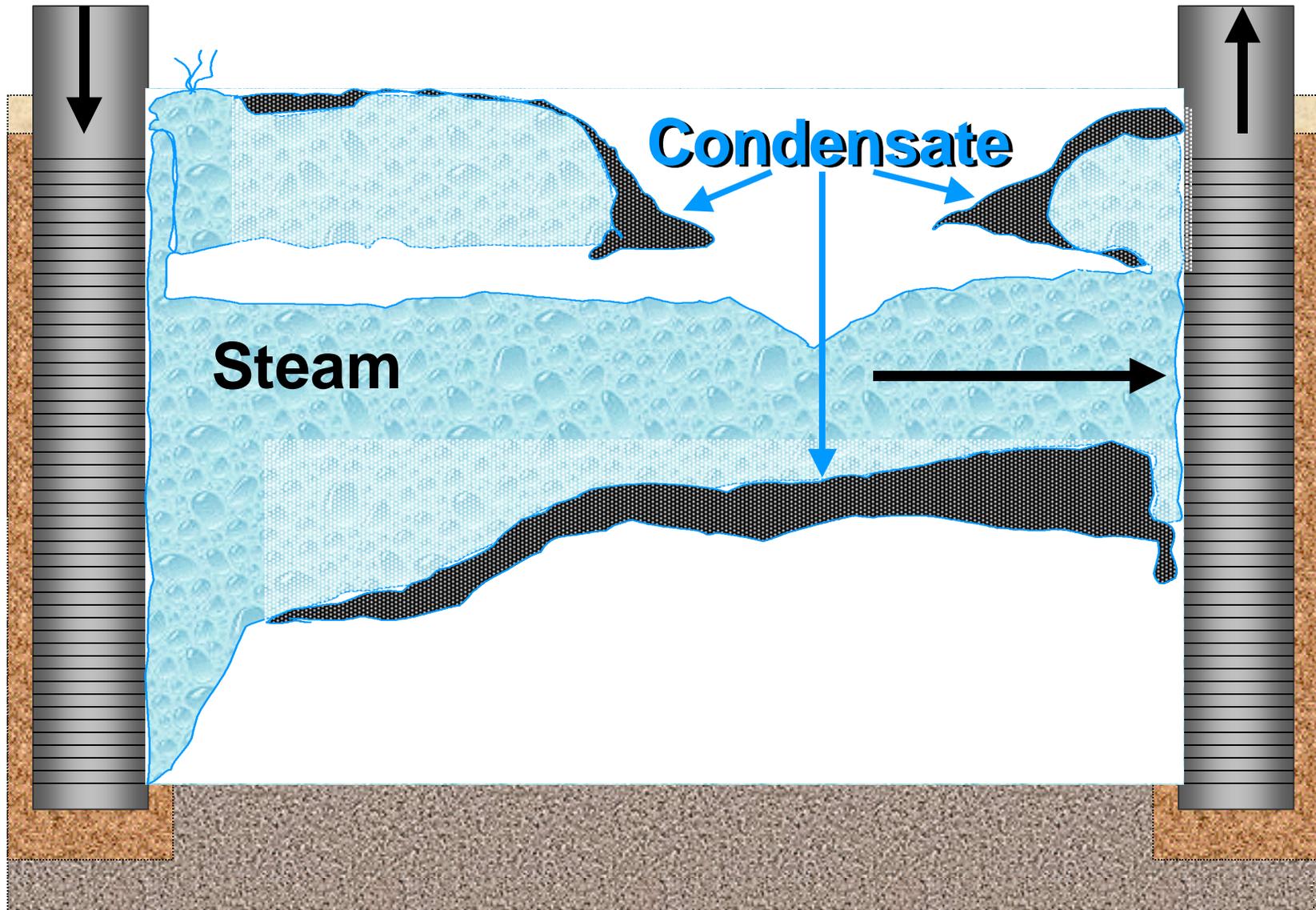
**Vacuum
Extraction**



**Steam
Injection**

“Steam Sweep”

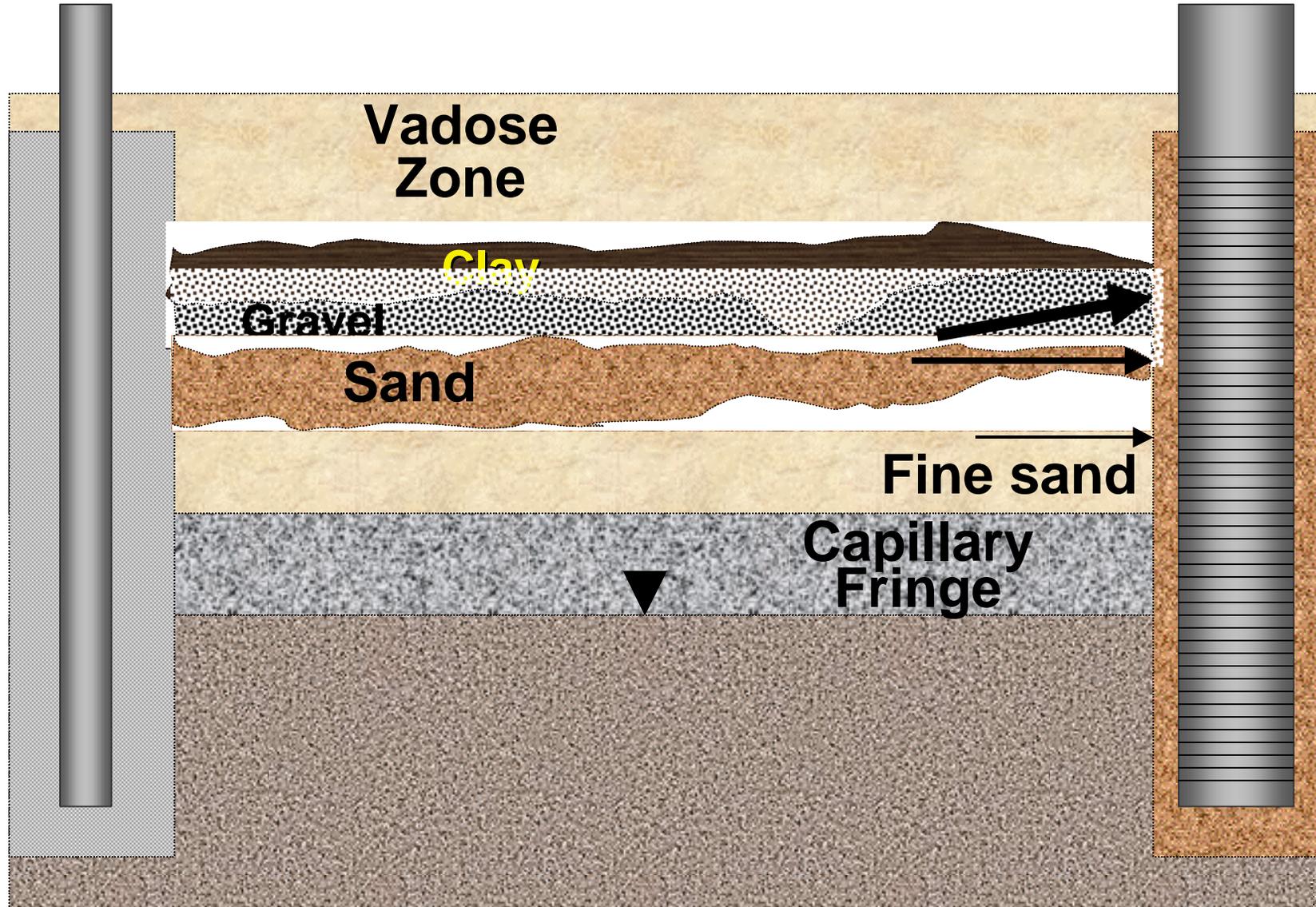
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Extraction**



**Heating
Electrode**

SVE Only

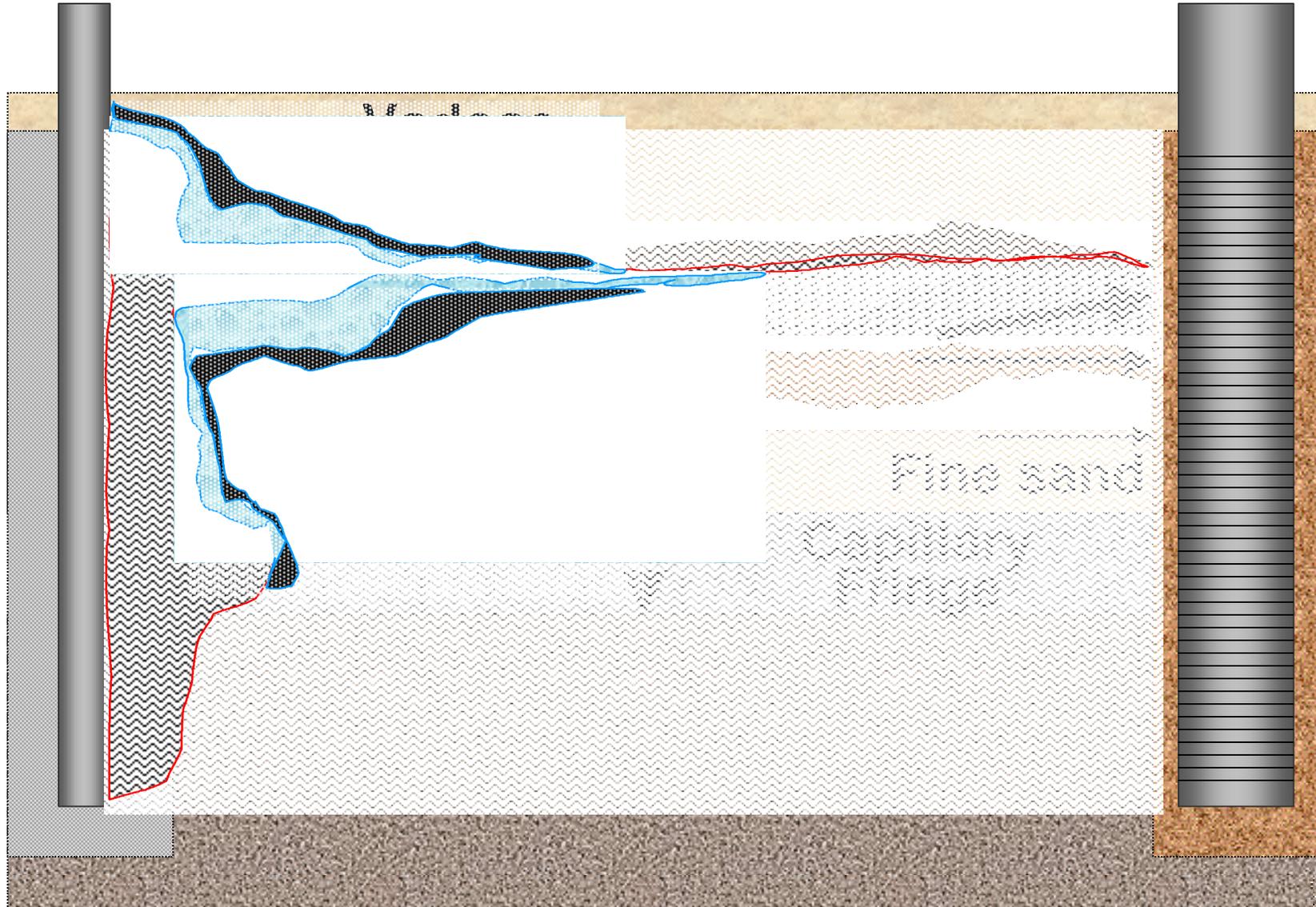
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Extraction**



**Heating
Electrode**

Early Heating

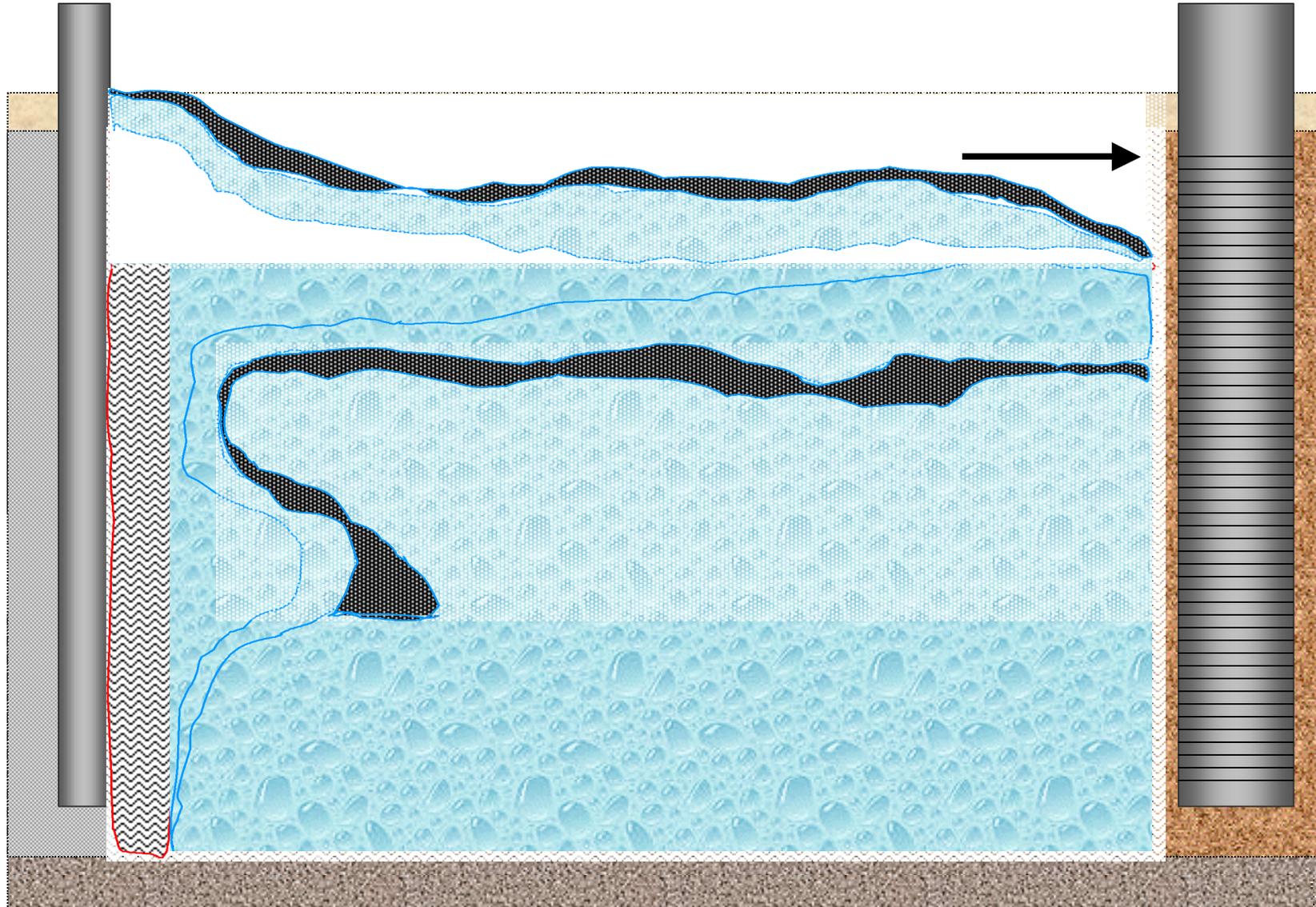
**Vacuum
Extraction**



**Heating
Electrode**

Mid-Heating

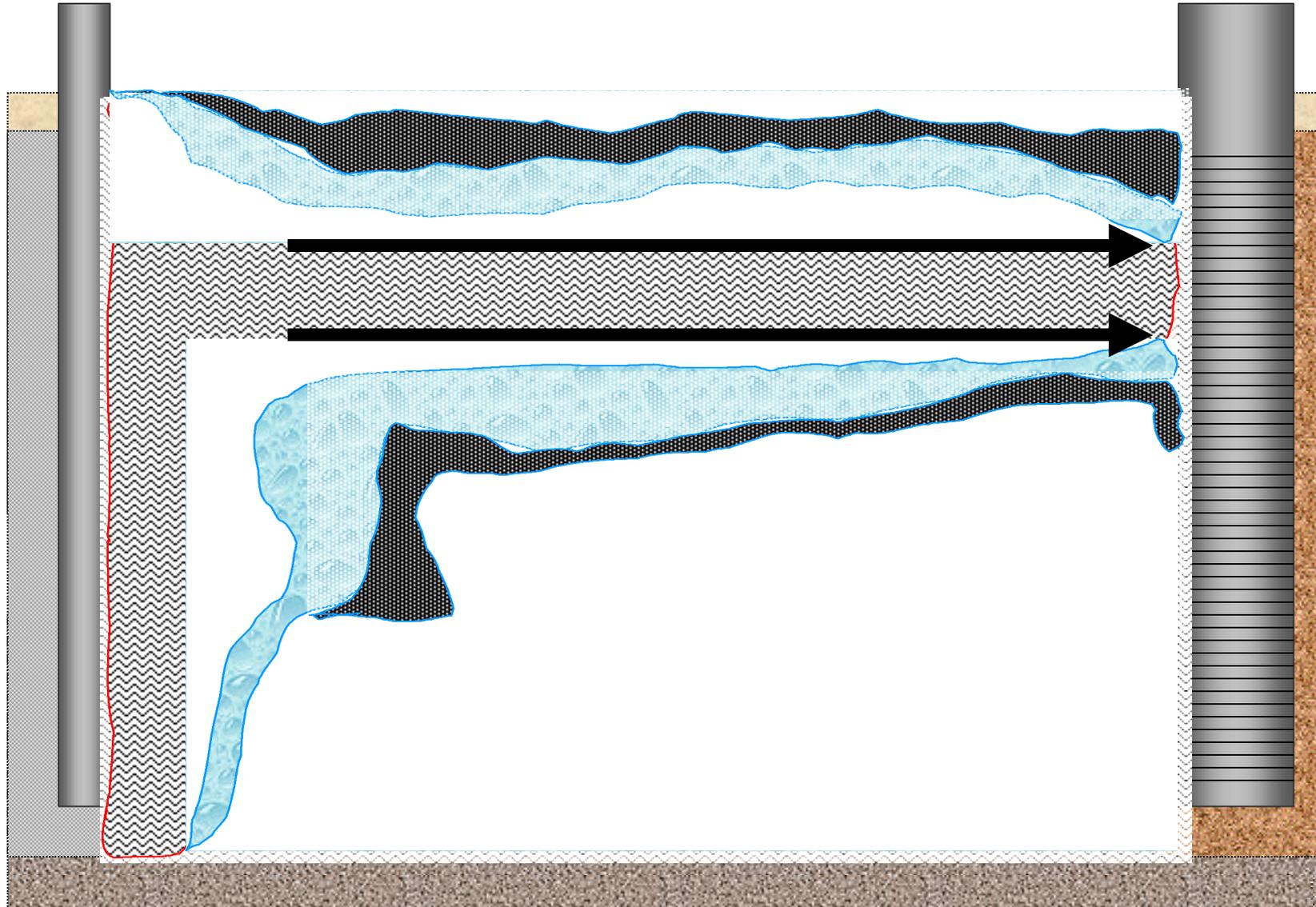
**Vacuum
Extraction**



**Heating
Electrode**

Final Heating

**Vacuum
Extraction**





Other Issues

- **Viability of modular approach**
- **Compatibility with on-site utilities**
- **Fugitive emissions**
- **Degree of mass removal - Enough?**
- **Risk to on-site workers**
- **Site characterization requirements to implement and evaluate**
- **Availability of specialized equipment**
- **How to collect representative samples**



Costs

- **How much do you have to spend?**

- **Very site-specific**
 - **Site complexity**
 - **Saturated zone impacts**
 - **Energy costs**
 - **\$50 - 300/yd³**



Summary

- **Use of thermal remediation increasing**
- **Capture of mobilized contaminant is the area of greatest concern**
- **Application to DNAPL impacted saturated zones appears particularly problematic**
- **Performance evaluation requires more consistent and rigorous testing methodologies**



Summary

- **Resistive heating may be more advantageous at silt or clay sites - Unique niche**
- **Modular approach common**
- **More sophisticated tracer and recovery tests would significantly improve safety and performance evaluation**
- **Buyer beware!**



References

Balshaw-Biddle, K.; Oubre, C. L.; Ward, C. H. (Editors): Dablow, J. F.; Johnson, P. C.; Pearce, J. A. (Authors). 2000. Steam and Electroheating Remediation of Tight Soils. Lewis Publishers, Boca Raton.